

Centres Of Mass Exam Questions MS (From OCR 4729)

Q1, (Jun 2005, Q1)

(i)	use of $h/4$	B1			
	com vert above lowest pt of contact	B1		can be implied	
	$r = 5 \times \tan 24^\circ$	M1			
	$r = 2.2$	A1	4	2.226	
(ii)	No & valid reason (eg $24^\circ \leftrightarrow 26.6^\circ$)	B1✓	1	✓ Yes if their $r \approx 2.5$	5

Q2, (Jan 2006, Q4)

(i)	horiz comps in opp direct	B1		at E & F	
	Right at E + Left at F	B1	2		
(ii)	$1.6 \times 9.8 \times 30 = 20X$ or $0.5 \times 30g + 0.7 \times 30g +$ $0.2 \times 60g = 20X$	M1 A1		or $10X + 1.6g \times 30 = 30X$ M(A) or $10X + (. . . = 470.4) = 30X$ M mark ok without g but 3 parts	
	$X = 23.5$ N	A1	3		
(iii)	$1.6 \bar{y} =$	M1		must be moments with vert dists	
	$20 \times 0.2 + 20 \times 0.2 + 40 \times 0.5$	A1		or $1.6 \bar{y} = 20 \times 0.2 \times 2 + 40 \times 0.7 (22.5)$	
	$\bar{y} = 17.5$ cm	A1	3		8

Q3, (Jun 2006, Q3)

(i)	$d = 2.25$ $h = 1.125$ or 1.12 or 1.13 or $9/8$	B1 B1	2	$3/8 \times 6$ OG (be generous) horizontal distance	
(ii)	$T_1 + T_2 = 12$ resolving vertically $T_1 \times 6 \cos 30^\circ = 12xh$ (their h) mom(O) (their h ok for A1) $T_1 = 2.60$ N or $3\sqrt{3}/2$ $T_2 = 9.40$ N ✓ $(12 - T_1)$ above ✓ depends on at least one of the M marks ($T_s > 0$)	M1 M1 A1 A1 A1✓	5	if not then next M1 ok or mom(A) $T_2 \times 6 \cos 30^\circ =$ $12(6 \cos 30^\circ - h)$ or $T_2 = 9.40$ or $T_1 = 2.60$ or ✓ $(12 - T_2)$	7

Q4, (Jan 2007, Q6)

(i)	com of Δ 4 cm right of C	B1			
	$1.5 \times 10 + 7 \times 20 = \bar{x} \times 30$	M1			
		A1			
	$\bar{x} = 5.17$	A1		$5 \frac{1}{6}$ $3 \frac{1}{6}$	
	com of Δ 6 cm above E	B1		or 3 cm below C	
	$4.5 \times 10 + 6 \times 20 = \bar{y} \times 30$	M1			
		A1			
	$\bar{y} = 5.5$	A1	8		
(ii)	$\tan \theta = 5.17/3.5$	M1		right way up and $(9 - \bar{y})$	
	55.9° or 124°	A1✓	2	✓ their $\bar{x} / (9 - \bar{y})$	
(iii)	$d = 15 \sin 45^\circ$ (10.61)	B1		dist to line of action of T	
	$Td = 30 \times 5.17$	M1		allow $T \times 15$ i.e. T vertical	
	$T = 14.6$	A1	3		13

Q5, (Jun 2007, Q8)

(i)	com of hemisphere 0.3 from O	B1	or 0.5 from base
	com of cylinder $h/2$ from O	B1	
	$0.6 \times 45 = 40 \times 0.5 + (0.8 + h/2) \times 5$ or	M1	or $40 \times 0.3 - 5 \times h/2 = 45 \times 0.2$
	$45(h+0.2) = 5h/2 + 40(h+0.3)$	A1	or $5(0.2 + h/2) = 40 \times 0.1$
	$27 = 20 + (0.8 + h/2) \times 5$	M1	solving
	$h = 1.2$	A1 6	AG
(ii)	1.2 T	B1	
	0.8 F	B1	
	$0.8F = 1.2T$	M1	
	$F = 3T/2$	A1 4	aef
(iii)	$F + T \cos 30^\circ$	B1	or $45 \times 0.8 \sin 30^\circ$
	$45 \sin 30^\circ$ must be involved in res.	B1	$T \times (1.2 + 0.8 \cos 30^\circ)$
	resolving parallel to the slope	M1	mom. about point of contact
	$F + T \cos 30^\circ = 45 \sin 30^\circ$ aef	A1	$45 \cdot 0.8 \sin 30^\circ = T(1.2 + 0.8 \cos 30^\circ)$
	$T = 9.51$	A1	
	$F = 14.3$	A1 6	16
or	$T + F \cos 30^\circ = R \sin 30^\circ$	B1	res. horizontally
(iii)	$R \cos 30^\circ + F \sin 30^\circ = 45$	B1	res. vertically
	$\tan 30^\circ = (T + F \cos 30^\circ) / (45 - F \sin 30^\circ)$	M1	eliminating R

Q6, (Jan 2009, Q3)

(i)	$140 \times X = 40 \times 70$	M1	
	$X = 20 \text{ N}$	A1	
	at F 20 N to the right	B1	inspect diagram
	at G 20 N to the left	B1 4	SR B1 for correct directions only
(ii)	$\bar{d} = (2 \times 40 \sin \Pi/2) \div 3\Pi/2$	M1	must be radians
		A1	
	$\bar{d} = 17.0$	A1	16.98 160/3\Pi (8/15\Pi m)
	$70 \bar{y} = 100 \times 60 + 217 \times 10$	M1	
		A1 ft	ft 200 + their \bar{d} or 2 + their \bar{d} (m)
	$\bar{y} = 117$	A1 6	116.7 10

Q7, (Jan 2010, Q3)

(i)	$\bar{u} = 0.2$ (from vertex) or 0.8 or 0.1 $0.5\bar{d} = 0.2 \times \bar{u} + 0.3 \times 0.65$	B1 M1 A1	com of conical shell
	$\bar{d} = 0.47$	A1 [4]	AG
(ii)	$s = 0.5$ $T \sin 80^\circ \times 0.5 = 0.47 \times 0.5 \times 9.8$	B1 M1 A1	slant height, may be implied
	$T = 4.68 \text{ N}$	A1 [4]	8

Q8, (Jun 2014, Q3)

(i)	<p>CoM of triangle = $\frac{1}{3} \times cv(12)$ from BD</p> $(80 + 60)x_G = 4(80) + 12(60)$ $x_G = 7.43 \text{ cm}$	<p>B1 M1 A1 A1 A1 [5]</p>	<p>OR $\frac{2}{3} \times cv(12)$ from C. CoM of triangle Table of values idea 7.42857... or $\frac{52}{7}$ cm</p>
(ii)	<p>$\tan \theta = (8 - x_G)/5$ $\tan \theta = 0.5714.../5$ $\theta = 6.52^\circ$</p>	<p>M1 A1ft A1 [3]</p>	<p>Using tan to find a relevant angle ft their x_G to target angle with the vertical 6.5198... Allow 6.5(0) from $x_G = 7.43$</p>

Q9, (Jun 2015, Q4)

(i)	<p>$2(8)\sin(\pi/2)/(3\pi/2)$</p> $(80 + 32\pi)x_G = 80(2) + 32\pi(4 + cv(\text{CoM}))$ $x_G = 5(.00) \text{ cm}$	<p>B1 M1 A1 A1ft A1 [5]</p>	<p>CoM of semi-circle (3.395305...); $(32/3\pi)$ Table of values idea to get an equation/expression, using any fixed axis Relative to the axis they are using; ft their CoM (5.004444492 cm)</p>
(ii)	<p>$4(20) = W(x_G \text{ from (i)} - 4)$ $4(20) = W(x_G \text{ from (i)})$ (Greatest) $W = 80 \text{ N}$ (Least) $W = 16 \text{ N}$</p>	<p>M1 A1ft A1ft A1 A1 [5]</p>	<p>Moments about E or A; allow wrong distance for either force ft on $cv(x_G)$; mg OK here; if $x_G < 4$ need $(4 - x_G \text{ from (i)})$ ft on $cv(x_G)$; mg OK here 79.64601393 from exact x_G; allow anything between 79.6 and 80 15.98579026 from exact x_G SC for masses found only, 4/5 for both 8.13 to 8.16 and 1.63</p>

Q10, (Jun 2016, Q3)

(i)	<p>CoM of one semicircular lamina is $\frac{4a}{\pi}, \frac{4a}{3\pi}$</p> $-\left(\frac{1}{2}\pi a^2\right)\left(\frac{4a}{3\pi}\right) + \left(\frac{1}{2}\pi(3a)^2\right)\left(\frac{12a}{3\pi}\right)$ $= \left(\frac{1}{2}\pi(3a)^2 - \frac{1}{2}\pi a^2\right)x_G$ $x_G = \frac{13a}{3\pi}$	<p>B1 M1 A1 A1 A1 [5]</p>	<p>oe, may be unsimplified, allow $\frac{4r}{3\pi}$ Table of values idea AG Correctly shown</p>
(ii)	<p>$3g\left(\frac{13a}{3\pi}\right) = (T \cos 40)(6a)$ $T = 8.82 \text{ N}$</p>	<p>M1 A1 A1 [3]</p>	<p>Moments equation in terms of a and T, with correct number of terms, dimensionally correct, resolving on T side of equation; if conflicting evidence about point taking moments mark to benefit of candidate. $T = 8.822960...$</p>
(iii)	<p>$X = T \cos 40$</p> <p>$Y = 3g + T \sin 40$</p> <p>$\tan \theta = \frac{35.0712...}{6.7587...}$</p> <p>$\theta = 79.1$ above horizontal (to the left)</p> <p>OR</p> <p>$x^2 = (3g)^2 + T^2 - 2 \times 3g \times T \times \cos 130$ Use of sine rule to find either of the missing angles $\theta = 79.1$ above horizontal (to the left)</p>	<p>B1 B1 M1 A1 [4] M1A1ft M1 A1</p>	<p>ft candidates value of T if substituted ($X = 6.758779...$) ft candidates value of T if substituted ($Y = 35.071289...$) Any relevant angle $\theta = 79.0919...$ (10.9 to the <u>upward</u> vertical); above or upwards may be implied by a correct diagram. $\theta = 79.0919...$ (10.9 to the <u>upward</u> vertical); above or upwards may be implied by a correct diagram.</p>